



# Phase transformations and surface characterization of the platinum-chromium coated system

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## Synopsis

This research involves the investigation of phase transformations in the platinum-chromium coated system. Single-layer 0.1  $\mu\text{m}$  platinum coatings were deposited via electron beam deposition on 99.98 percent pure chromium substrates. Specimens were subjected to systematic heat treatment in a vacuum furnace at 900°C for up to 20 hours. Phase formation and the changes in surface morphology were investigated by X-ray diffraction (XRD) and scanning electron microscopy (SEM). Both CrPt and Cr<sub>3</sub>Pt phases are formed during heat treatment for different times at 900°C. Significant changes in the morphology of this coated system were detected after heat treatment at 900°C for 20 hours.

## Keywords

Platinum-chromium system, platinum coating, chromium substrate, phase formation, surface morphology.

## Introduction

The platinum-chromium (Pt-Cr) system is used in many applications, including magneto-optics and micro-electronics. Platinum (Pt) can be used for ohmic contacts, and when alloyed with chromium (Cr), the reliability of this contact is greatly improved<sup>1</sup>. Pure chromium has a favourable strength-density ratio with excellent corrosion resistance. However, this metal has numerous problems in production, shaping, and joining<sup>2</sup>. Its excellent corrosion resistant properties and high melting temperature make it useful in functional coatings and for improving wear and corrosion resistance<sup>2</sup>. Coated systems offer the potential to control experimental parameters such that specific phases can be formed with desired mechanical properties<sup>3,4</sup>. The literature on platinum-chromium coated systems is limited, and thus further research should be conducted on this coated system.

A solid-state interfacial reaction occurs upon heat treatment, resulting in diffusion of Pt and Cr to form various phases. Diffusion in thin films differs from that in bulk systems due to differences in structure and grain

boundary activation energy<sup>5</sup>. For diffusional phase transformations, thin films exhibit characteristics such as sequential formation of phases, which are not seen in bulk diffusion couples<sup>3,4</sup>. This can also bring about the formation of ordered intermetallic compounds, which can alter the mechanical properties of the material<sup>6</sup>. This study aims to determine the sequence of phase formation and development of surface morphology for the platinum-chromium coated system, with a view to contributing to electronic device optimization<sup>7</sup>. This work is also aimed at developing a better understanding of the thermodynamic and kinetic description of the formation of phases in this system.

The thermodynamic description of the Pt-Cr system predicts the Cr<sub>3</sub>Pt phase to form initially which is in accordance with the effective heat of formation (EHF) model described below. The Cr<sub>3</sub>Pt phase has a more negative heat of formation than the CrPt and Pt<sub>3</sub>Cr phases<sup>3</sup>. This is seen in Figures 1(a) and (b), which portray the equilibrium phase diagram and the effective heat of formation diagram respectively.

## The effective heat of formation model<sup>3,4</sup>

Pretorius *et al.*<sup>3,4</sup> describes an efficient model that makes accurate predictions on phase formation. The EHF model is a thermodynamic model used to predict the first and sequential

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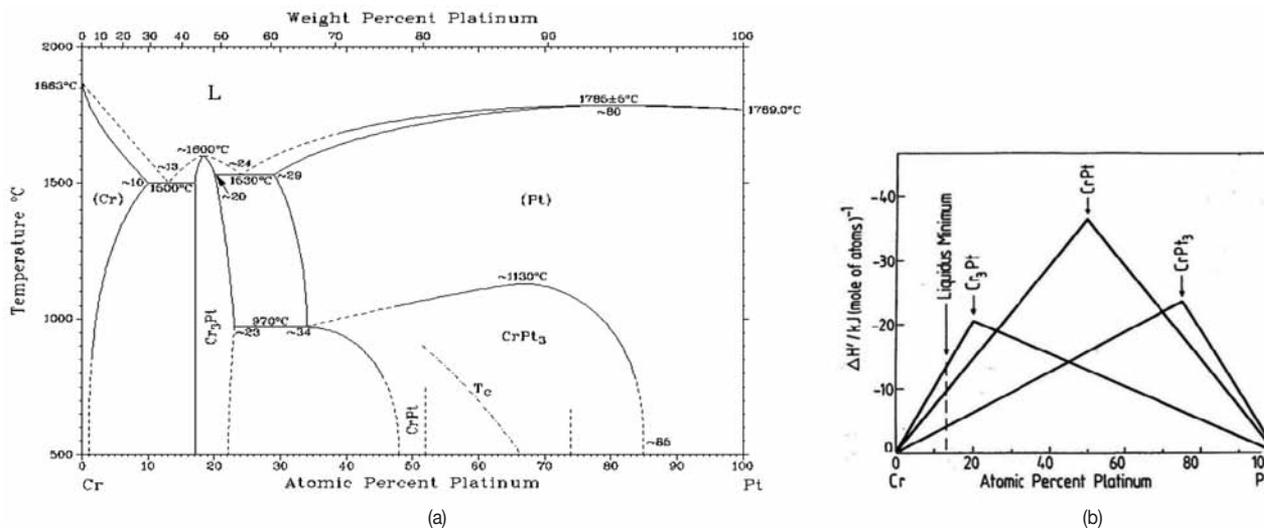


Figure 1—(a) The equilibrium phase diagram of the platinum-chromium system showing two liquidus minima, and (b) the effective heat of formation diagram of the platinum-chromium system<sup>3,4</sup>

formation of phases. This model makes use of thermodynamic data such as a modified heat of formation ( $\Delta H'$ ), which is dependent on the effective concentrations (Equation [1]) of the elements reacting at the interface of the substrate and coating. The activation energy for solid-state interdiffusion is directly proportional to the melting point of the solid and thus determines the mobility of the atoms during diffusion<sup>3,4</sup>. The effective concentration is thus taken at the composition of the liquidus minimum as this is the point of highest mobility of atoms at the interface.

$$\Delta H^1 = \Delta H^0 x \left( \frac{\text{effective concentration limiting element}}{\text{compound concentration limiting element}} \right) \quad [1]$$

where  $\Delta H^0$  is the heat of formation of the compound phase.

The rules for predicting phase formation in this model state that 'The first compound phase to form during metal-metal interaction is the phase with the most negative effective heat of formation at the concentration of the lowest temperature eutectic of the binary system' and 'the next phase to form at the growth interface is the next phase richer in the unreacted element'<sup>3,4</sup>. In Figure 1 (a) shows that two liquidus minima exist for the Pt-Cr system at approximately similar temperatures (1 500°C at ~13 at.% Pt and 1 530°C at ~24 at.% Pt) and thus the prediction of the first phase in this system is more uncertain<sup>3,4</sup>. Figure 1 (b) predicts the initial phase formation to be the  $\text{Cr}_3\text{Pt}$  phase using the liquidus minimum at 13 at.% Pt and the next phase formed to be CrPt. However, due to the high affinity of chromium for oxygen, it could be expected that the effective concentration of this system is shifted to the Pt-rich side on the EHF diagram<sup>3,4</sup>. Thus the liquidus minimum at 24 at.% Pt would be used and the first phase would be predicted to be the CrPt phase<sup>3,4</sup>.

### Experimental procedure

Pure platinum (99.99 percent) was used as a target material for the electron beam deposition of 0.1  $\mu\text{m}$  platinum coatings on 99.98 percent pure chromium substrates. Cast chromium pieces were cut, ground, and polished to a mirror finish using a colloidal silica suspension. Substrates were then cleaned in different solutions such as methanol, ethanol, acetone, distilled water, and hydrofluoric acid in an ultrasonic bath prior to deposition. Platinum was then deposited with the use of an evaporation system and an electron beam source. After deposition, the specimens were subjected to systematic heat treatments in a vacuum furnace at a high temperature of 900°C.

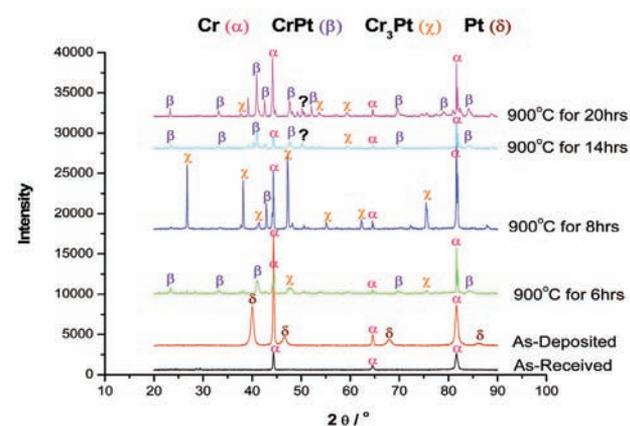


Figure 2—X-ray diffraction patterns after 900°C heat treatments for up to 20 hours showing the existence of the  $\text{Cr}_3\text{Pt}$  and CrPt phases at different times

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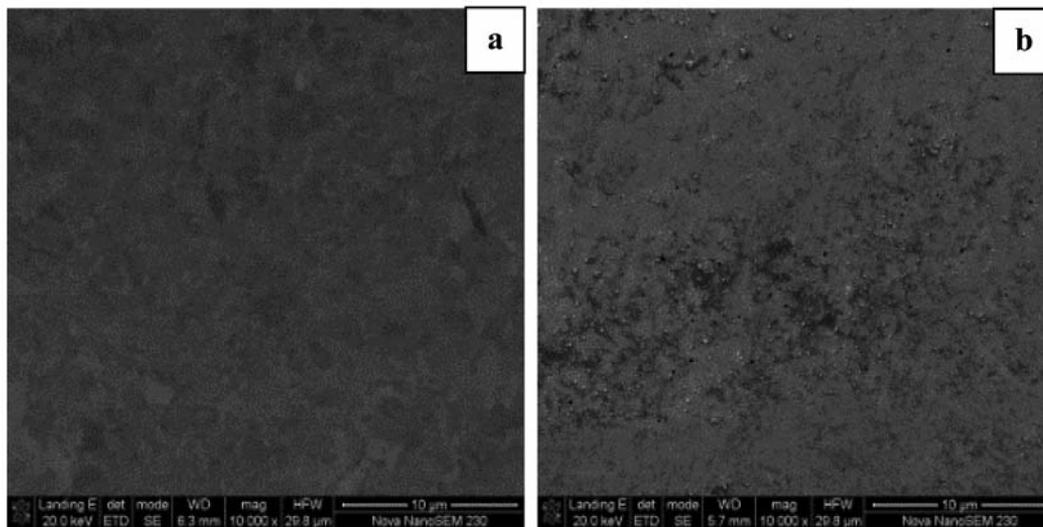


Figure 3—SEM images of (a) as-received, and (b) as-deposited pure chromium substrates, with 0.1 μm platinum coating displaying a smooth morphology

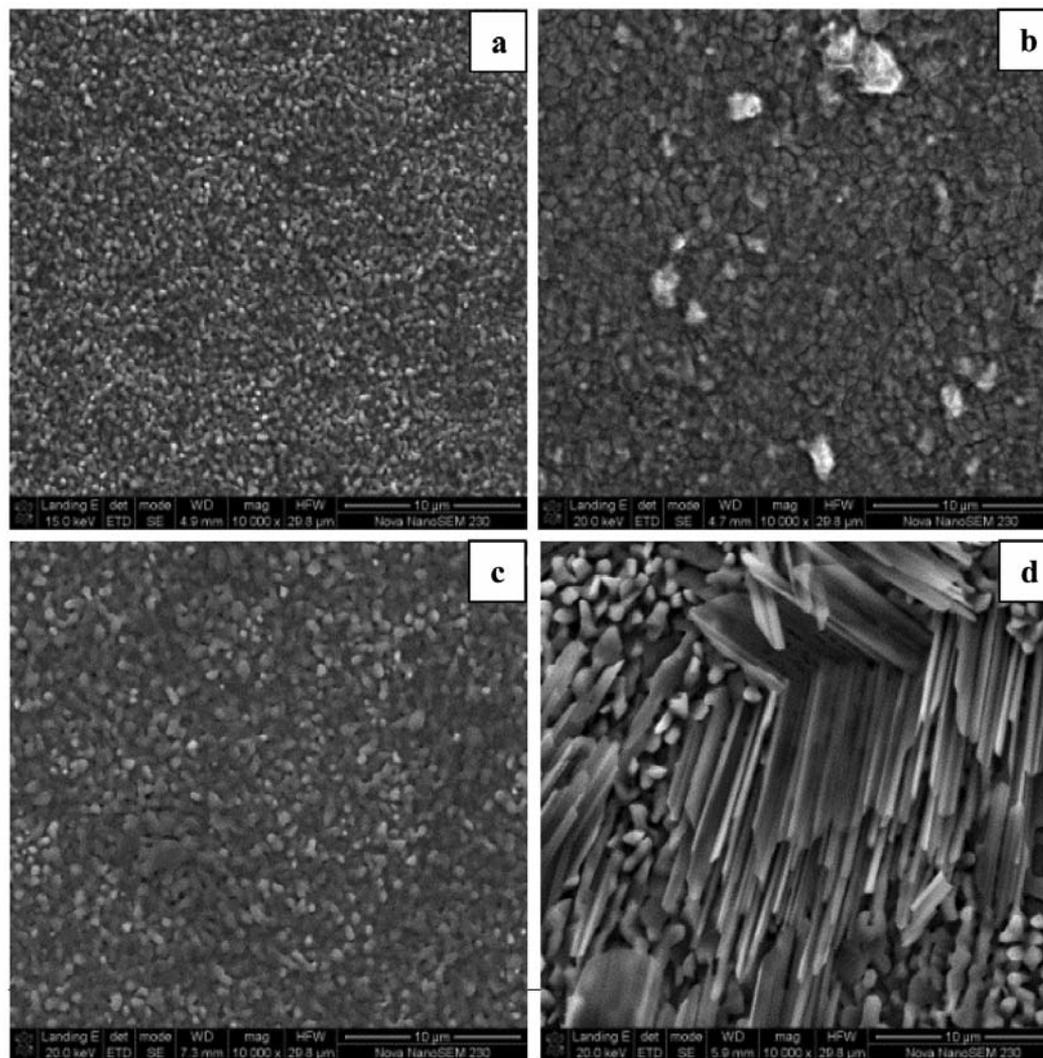


Figure 4—SEM images of pure chromium substrates with 0.1 μm platinum coating heat treated at 900°C for (a) 6 h, (b) 8 h, (c) 14 h and (d) 20 h displaying an increase in surface roughness with respect to time and the formation of needle-like crystals

## Phase transformations and surface characterization of the platinum-chromium coated system

Phase formation and the changes in surface morphology were investigated by X-ray diffraction (XRD) and scanning electron microscopy (SEM). These were used as complementary techniques in this study. A BRUKER ADVANCE-8 diffractometer was used with  $\text{CuK}\alpha$  radiation at 40 kV and 40 mA for XRD, and a NOVA NANOSEM 230 at 20 kV and a magnification of 10 000 $\times$  was used for microscopy images and energy dispersive X-ray spectroscopy (EDX).

### Results and discussion

#### X-ray diffraction

In Figure 2 the XRD patterns of the platinum-coated chromium substrates heat treated at 900°C for different times are displayed. As-received plots show Cr peaks, whereas as-deposited plots show both Cr and Pt peaks. The CrPt and  $\text{Cr}_3\text{Pt}$  phases are observed at all times taken into consideration at this temperature; however, a significant difference is noted at the 8 hour time interval. The volume fraction of the  $\text{Cr}_3\text{Pt}$  phase is observed to be the highest at this time, and longer annealing periods caused a decrease in the  $\text{Cr}_3\text{Pt}$  volume fraction. It is also observed that after long annealing periods the volume fraction of the CrPt phase is increased. This is particularly pronounced after annealing for 20 hours. It is clear that the volume fractions of these phases change with increasing annealing time. Since only a few time intervals were considered, a definite phase formation sequence cannot be predicted according to the EHF model. It should also be noted that there are peaks that could not be identified due to the lack of information in the XRD database. Further studies of the phases in this system need to be conducted in order to provide an accurate prediction of phase formation sequence.

#### Electron microscopy

The surface morphology is smooth before and after electron beam deposition. Figure 3 shows SEM images of (a) as-received and (b) as-deposited specimens. After heat treatment at high temperatures, a solid state interfacial reaction occurs, resulting in diffusion between the platinum coating and chromium substrate. Figures 4 (a) to (d) show SEM images of platinum-coated chromium substrates after heat treatment at 900°C from 6 hours up to 20 hours. Vast differences in morphology are evident with respect to time, with a general increase in coating roughness. Figures 4 (a) to (c) display a granular morphology that progressively

increases in size with time. In Figure 4 (d) chromium-rich needle-like crystals are formed on the surface of the coating, with EDX analysis showing a composition of 100 at.% Cr in these crystal regions. The crystals protrude from the surface in different orientations after annealing at an approximate angle of 45°.

### Summary and conclusion

Phase transformations in the Pt-Cr coated system occur as per the platinum-chromium equilibrium phase diagram and include the  $\text{Cr}_3\text{Pt}$  and CrPt phases. The sequence of phase formation at the interface between the Cr and Pt at 900°C cannot, however, be determined in this study due to the few time intervals being considered. The coating morphology is significantly affected by heat treatment, where large needle-like crystals are formed on top of the coating surface. These results have not been previously observed and thus serve as a basis for further study on this system. This would entail the effects of this morphology on the mechanical properties of Pt-Cr coatings and the continued study of phase formation.

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