



Removal of heavy metals using cassava peel waste biomass in a multi-stage countercurrent batch operation

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Synopsis

This paper presents a study of the removal of cobalt (Co^{2+}), chromium (Cr^{3+}), and vanadium (V^{3+}) from synthetic effluent solution using cassava waste biomass. Test work was carried out in a multi-stage countercurrent batch system. Single and ternary metal ion systems were studied. A feed inlet concentration of 100 mg/L for each metal ion system was contacted with 0.5 g of cassava waste biomass. The target concentration in the final outlet stream was set against the South African Department of Water and Forestry (DWAF) standards. The results showed that the adsorption capacity was slightly lower for ternary metal ion systems than for single metal ion systems. This was attributed to the greater competition among the metal ions for the occupancy of the binding surfaces on the cassava waste in the ternary systems. Eight adsorption stages were required to meet the targeted limit of 0.5 mg/L for Co^{2+} set by the DWAF. The Cr^{3+} system needed six stages to obtain the targeted limit of 0.1 mg/L, while the V^{3+} system required four stages to attain the target limit of 0.2 mg/L. In general, cassava waste biomass adsorbed the metal ions in the following order: $\text{V}^{3+} > \text{Cr}^{3+} > \text{Co}^{2+}$.

Keywords

heavy metals, wastewater, biosorption, cassava waste, biomass, multi-stage, countercurrent, batch.

Introduction

Wastewaters from many sources, such as the metallurgical, tannery, chemical manufacturing, mining, and battery manufacturing industries, contain toxic heavy metals. The concentrations of some of the toxic metals in these effluents are sometimes higher than permissible discharge levels. Discharge of the contaminated wastewater into the environment would, therefore, create a significant environmental hazard, including impacts on human, animal, and plant health (Matouq *et al.*, 2005). According to the South African Department of Water Affairs and Forestry (DWAF) (2005), the permissible discharge limits for chromium, cobalt, and vanadium are 0.1, 0.5, and 0.2 mg/L, respectively. Therefore, it becomes necessary to remove these heavy metals from wastewaters by an appropriate treatment process before releasing them into the environment (Meena *et al.*, 2005).

Several conventional chemical and physical methods have been developed and used to remove high concentrations of heavy metals from wastewater effluents, including (but not

limited to) precipitation, solvent extraction, ion exchange, reverse osmosis, oxidation/reduction, sedimentation, filtration, and electrochemical techniques (Volesky, 2001; Feng *et al.*, 2010; Nassar, 2010; Shen *et al.*, 2009; Song *et al.*, 2011; Ahmadi *et al.*, 2014). However, most of these methods have high capital and operational costs, low metal removal efficiency at low concentrations, and generate toxic sludge that requires additional treatment (Ahmadi *et al.*, 2014; Motouq *et al.*, 2015). Therefore, a lot of effort has been directed at the development of economical methods for the removal of toxic heavy metals from wastewater effluents.

The use of biological-based technologies such as biosorption for removal of heavy metals from wastewater effluents has recently become the subject of considerable interest because of the low cost and high efficiency associated with the process (Arminia *et al.*, 2015). Previous studies by the authors have shown that cassava peel waste is a potentially useful biosorbent for treating wastewater contaminated with Co^{2+} , V^{3+} , and Cr^{3+} ions (Ndlovu *et al.*, 2013; Simate and Ndlovu, 2014; Seepe, 2014). Cassava is a perennial woody shrub, grown as an annual crop, and serves as a major source of low-cost carbohydrates for populations in the humid tropics (O'Hair, 1995; Simate *et al.*, 2013; Adetunji *et al.*, 2015). In the past, the largest producer of cassava was Brazil, followed by Thailand, Nigeria, the DRC, and Indonesia (O'Hair, 1995; Adetunji *et al.*, 2015), but today Nigeria is the largest producer (Adetunji *et al.*, 2015). So far, not much effort has been made to control or manage the enormous quantities of wastes arising from processing cassava tuber into its

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various products, which are abundant and available in all seasons (Seepe, 2014). Since cassava waste has no economic value, its conversion into biosorbents would ultimately economically benefit the millions of cassava producers. Indeed, the economic utilization of cassava waste would not only provide a solution to the environmental nuisance that it poses, but would create employment and improve local economies (Ndlovu *et al.*, 2013).

Since the manner in which the biomass contacts with the solution to be treated is of particular significance for large-scale treatment of water, initial studies by the authors involved, firstly, batch equilibrium relating to adsorbate, adsorbent, and operating conditions (Ndlovu *et al.*, 2013). This was followed by heavy metal removal studies in a column packed with immobilized cassava waste pellets (Simate and Ndlovu, 2014). Column-type continuous flow operations have an advantage over batch-type operations because the rates of adsorption depend on the concentration of solute in the solution being treated. For column operation, the biomass is continuously in contact with a fresh solution. Consequently, the concentration in the solution in contact with a given layer of biomass in a column changes very slowly. In batch treatment, the concentration of solute in contact with a specific quantity of biomass decreases much more rapidly as adsorption proceeds, thereby decreasing the effectiveness of the adsorbent for removing the solute (Zhou, 2013).

However, the main limitations of the two studies are: (1) batch systems are usually limited to the treatment of small quantities of wastewater (Bharathi and Ramesh, 2013), and data obtained from such systems may not be applicable directly to most treatment systems (such as column operations) where the contact time is not sufficient for the attainment of equilibrium (Zulfadhly *et al.*, 2001; Vinodhini and Das, 2010; Vimala *et al.*, 2011; Bharathi and Ramesh, 2013); and (2) fixed-bed column studies are characterized by clogging and subsequent release of adsorbent into the treated wastewater (Amirnia *et al.*, 2015), and immobilization of biomass also causes mass transfer limitations by hindering the access of the metals to the biosorbent sites compared to suspended biosorbents (Tsezos, 1990; Cassidy *et al.*, 1996). Furthermore, the regeneration capacity of immobilized biomass is limited, thus there is need for biomass to be replaced frequently, which is a costly process (Amirnia *et al.*, 2015). However, continuous operation is the only viable way of treating large volumes of wastewater in a reasonable time, and this is where bench-scale batch biosorption studies are limited in their scope (Amirnia *et al.*, 2015).

Based on the authors' earlier work on the removal of Co^{2+} , V^{3+} , and Cr^{3+} ions using cassava waste biomass in a batch system (Ndlovu *et al.*, 2013), metal adsorption using a multi-stage countercurrent batch system was investigated in this study. Multi-stage countercurrent adsorption operations

are superior to both batch and fixed bed operations because countercurrent flow maximizes the average driving force for mass transfer between the fluid and the adsorbent (Seepe, 2014). This technique involved contacting the metal ion solution with the cassava waste biomass in a series of gently agitated tanks for a sufficient retention time. The cassava and metal ion solution were transferred in a countercurrent flow arrangement. The schematic diagram for multi-stage batch adsorption is shown in Figure 1. In multi-stage countercurrent batch adsorption, the solution to be treated contains $L \text{ dm}^3$ solution and the concentration of heavy metals is reduced in each stage from C_{n-1} to $C_n \text{ mg/dm}^3$. The amount of biomass added is $B \text{ g}$ and the heavy metal concentration on the biomass is increased from q_{n+1} to $q_n \text{ mg/g}$ of biomass.

Materials and methods

Preparation of cassava waste biomass

The cassava tubers were obtained from local wholesalers in South Africa and were prepared as described by Ndlovu *et al.* (2013). In summary, cassava tubers were carefully peeled and the dried cassava peel waste was ground to $100 \mu\text{m}$ using a blender. Subsequently, the ground cassava peel waste was treated with nitric acid. Finally, sulphhydryl groups (or thiol groups) were introduced onto the cassava biomass using thioglycolic acid solution in the presence of hydroxylamine.

Multi-stage countercurrent biosorption operation

As illustrated in Figure 1, the multi-stage countercurrent biosorption was operated batchwise. About 0.5 g of cassava waste biomass was contacted with 100 mL of the influent solution in each reactor. The concentration of each metal ion in the inlet solution stream was 100 mg/L . Tests were conducted for single and ternary metal ion systems. Mixing was provided by agitation at 150 r/min . After 30 minutes, agitation was stopped and the biosorbent separated from metal ion solution by filtration. The biosorbent and effluent solutions were then transferred to the next respective reactors in a countercurrent manner. This procedure was followed until the final effluent was transferred to the discharge tank from reactor n . The saturated spent biomass emerging from the first reactor was transferred to the regenerator, in which the adsorbed metals were removed, and the biomass was subsequently reactivated and then returned to the adsorption circuit. The main advantage of this process is that the adsorbent can be regenerated as soon as its role in the adsorption step has been completed. Thus, in theory at least, the inventory of the adsorbent can be kept to a minimum. The quantity of adsorbent required for a given separation can also be reduced by increasing the number of stages. However, the possibility of regeneration and re-use of the

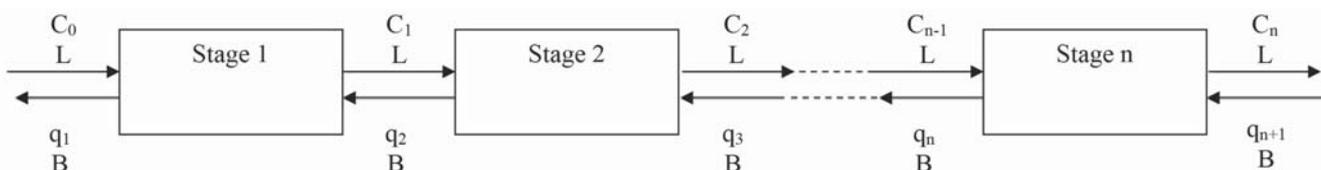


Figure 1 – Schematic diagram of multi-stage countercurrent batch adsorption

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cassava biomass was beyond the scope of this study. In practice, the heavy metals eluted from the cassava biomass could be further concentrated and/or used as an input in other hydrometallurgical processes.

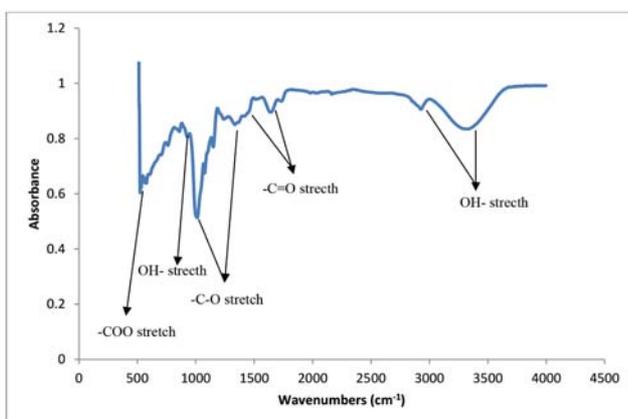
Results and discussion

Fourier transform infrared (FTIR) spectroscopy was used to identify the presence or absence of functional groups on the surface of cassava peel waste biomass before and after thiolation. Figure 2 shows the obtained FTIR spectra. As can be seen from Figure 2(a) and (b), the major difference between the two biomasses is the presence of the sulphhydryl group (-SH), which proves that thiolation process adds sulphhydryl functional groups on the cassava peel biomass (Ndlovu *et al.*, 2013; Simate and Ndlovu, 2015). Other differences between treated and untreated cassava biomass were reported by Ndlovu *et al.* (2013). For example, the BET surface areas obtained were in the following order: untreated < 0.5 M acid treated < 1 M treated, and both the pore volume and pore size were in the following order: untreated > 0.5 M acid treated > 1 M treated. The point of zero charge (pzc) for the untreated and treated cassava peel biomass was determined as 4.9 and 3.1, respectively. This shows that the functional groups on untreated cassava

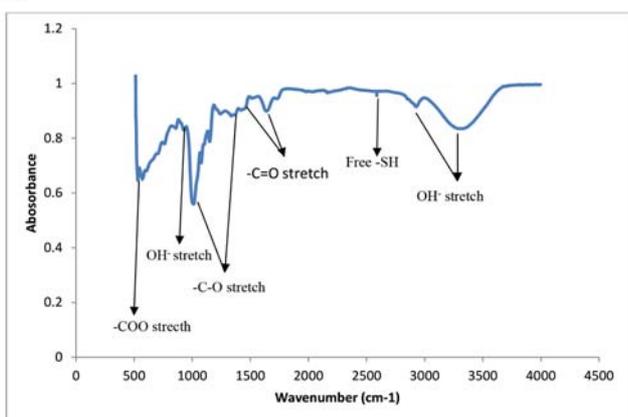
peel biomass are weakly acidic (or more basic) than the functional groups on treated cassava peel biomass. Therefore, the pzc results confirm that more acidic functional groups were incorporated into the cassava peel biomass during thiolation. These results concur well with the results shown in Figure 2(b), which shows the introduction of an acidic sulphhydryl group after thiolation.

Tables I–VI show the results of a series of adsorption tests, and the number of stages required to reduce the heavy metals in this study to acceptable drinking water standards as set by the DWAF. Tables I and II show the adsorption of Co^{2+} in single and ternary systems, respectively. Eight stages of Co^{2+} removal were needed to meet the targeted limit of 0.5 mg/L in the effluent discharge. The effluent solution obtained after the 8th stage contained 0.04 and 0.05 mg/L Co^{2+} for single and ternary systems, respectively. Tables III and IV show that the adsorption of Cr^{3+} needed six stages to obtain the targeted limit of 0.1 mg/L. For single system and ternary system, 0.04 and 0.05 mg/L were obtained, respectively. For V^{3+} , the effluent solution at the end of the 4th stage contained 0.01 and 0.02 mg/L for single and ternary systems, respectively (see Tables V and VI), with a target limit of 0.2 mg/L. In all cases, the adsorption capacity was slightly lower for the ternary metal ion system as compared to the single metal ion system. This may be attributed to the greater competition between the metal ions for the occupancy of the binding surfaces on the cassava waste biomass (Ndlovu *et al.*, 2013). Generally, the biosorption efficiency increased in the order $\text{Co}^{2+} < \text{Cr}^{3+} < \text{V}^{3+}$. These results are in agreement with our previous batch studies (Ndlovu *et al.*, 2013) and column studies (Simate and Ndlovu, 2014). The differences (or variations) are attributed to the metal ions' affinity towards the biosorbent (Mohan and Sreelakshmi, 2008), and this depends on the ionic radius and electropositive charges on the ions (Reddad *et al.*, 2002).

This study showed that the adsorption efficiency obtained in the multi-stage countercurrent system is higher than that obtained in our study of the batch system, implying that there is a limited number of active binding sites on the



(a)



(b)

Figure 2 – Fourier transform infrared spectra of cassava biomass: (a) before thiolation, (b) after thiolation (Ndlovu *et al.*, 2013)

Table I

Adsorption of cobalt onto acid-treated cassava waste biomass using batch countercurrent operation: single metal ion system, initial Co^{2+} concentration 100 mg/L

No. of stages	Final concentration (mg/L)	Metal uptake (related to effluent movement) (mg/g)	Metal uptake (related to cassava movement) (mg/g)	% recovery per stage
Tank 1 exit	43.02	11.40	19.89	56.97
Tank 2 exit	30.58	2.49	19.21	28.93
Tank 3 exit	25.42	1.03	18.32	16.89
Tank 4 exit	19.91	1.10	17.30	21.66
Tank 5 exit	10.99	1.78	15.92	34.71
Tank 6 exit	7.89	0.62	14.78	39.31
Tank 7 exit	3.46	0.89	13.78	56.17
Tank 8 exit	0.04	0.68	11.40	98.84

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Table II

Adsorption of cobalt onto acid-treated cassava waste biomass using batch countercurrent operation: ternary metal ion system, initial metal ion concentration 100 mg/L

No. of stages	Final concentration (mg/L)	Metal uptake (related to effluent movement) (mg/g)	Metal uptake (related to cassava movement) (mg/g)	% recovery per stage
Tank 1 exit	45.32	10.94	20.04	54.68
Tank 2 exit	35.13	2.04	19.26	22.50
Tank 3 exit	26.15	1.80	18.37	20.52
Tank 4 exit	20.78	1.07	17.20	32.3
Tank 5 exit	11.67	1.82	15.84	41.74
Tank 6 exit	8.17	0.70	14.77	54.74
Tank 7 exit	3.69	0.90	12.96	54.77
Tank 8 exit	0.05	0.73	10.94	98.64

Table III

Adsorption of chromium onto acid-treated cassava waste biomass using batch countercurrent operation: single metal ion system, initial Cr³⁺ concentration 100 mg/L

No. of stages	Final concentration (mg/L)	Metal uptake (related to effluent movement) (mg/g)	Metal uptake (related to cassava movement) (mg/g)	% recovery per stage
Tank 1 exit	38.15	12.37	19.99	61.86
Tank 2 exit	28.01	2.03	18.98	26.54
Tank 3 exit	20.01	1.60	17.62	28.52
Tank 4 exit	10.18	1.97	16.00	40.58
Tank 5 exit	5.13	1.01	14.40	56.89
Tank 6 exit	0.04	1.02	12.37	99.24

Table IV

Adsorption of chromium onto acid-treated cassava waste biomass using batch countercurrent operation: ternary metal ion system, initial metal ion concentration 100 mg/L

No. of stages	Final concentration (mg/L)	Metal uptake (related to effluent movement) (mg/g)	Metal uptake (related to cassava movement) (mg/g)	% recovery per stage
Tank 1 exit	40.16	11.97	20.28	59.84
Tank 2 exit	32.50	1.53	19.08	19.81
Tank 3 exit	21.74	2.15	17.65	33.10
Tank 4 exit	13.26	1.70	15.95	39.02
Tank 5 exit	6.13	1.43	13.80	53.78
Tank 6 exit	0.05	1.22	11.97	99.35

Table V

Adsorption of vanadium onto acid-treated cassava waste biomass using batch countercurrent operation: in single metal ion system, V³⁺ concentration 100 mg/L

No. of stages	Final concentration (mg/L)	Metal uptake (related to effluent movement) (mg/g)	Metal uptake (related to cassava movement) (mg/g)	% recovery per stage
Tank 1 exit	34.71	13.06	20.00	65.29
Tank 2 exit	18.13	3.32	18.98	47.78
Tank 3 exit	5.13	2.60	16.38	71.75
Tank 4 exit	0.01	1.02	13.06	99.90

Table VI

Adsorption of vanadium onto acid-treated cassava waste biomass using batch countercurrent operation: metal ion ternary system, initial metal ion concentration 100 mg/L

No. of stages	Final concentration (mg/L)	Metal uptake (related to effluent movement) (mg/g)	Metal uptake (related to cassava movement) (mg/g)	% recovery per stage
Tank 1 exit	38.85	12.23	20.00	61.15
Tank 2 exit	21.61	3.448	18.60	44.30
Tank 3 exit	6.99	2.924	15.67	67.71
Tank 4 exit	0.02	1.394	12.23	99.74

adsorbent for metal adsorption in a batch system. However, in the multi-stage system, a somewhat weak solution is in contact with a biomass that has more active binding sites as it moves up the train from last stage to the first stage, hence higher recoveries were obtained.

Conclusions

The required discharge limits were obtained for all metals using multi-stage countercurrent batch adsorption system with cassava peel waste biomass as biosorbent. The minimal accepted limits for Co²⁺, Cr³⁺ and V³⁺ discharge were reached in 8, 6, and 4 stages, respectively. Thus, in general, cassava waste biomass adsorbed the metal ions in the following order: V³⁺ > Cr³⁺ > Co²⁺. The adsorption efficiency obtained in the multi-stage countercurrent system was higher than that achieved previously in a batch process.

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