

Development of beneficiation processes for low-grade manganese ores for the ferroalloy industry

By D.A. Barrett

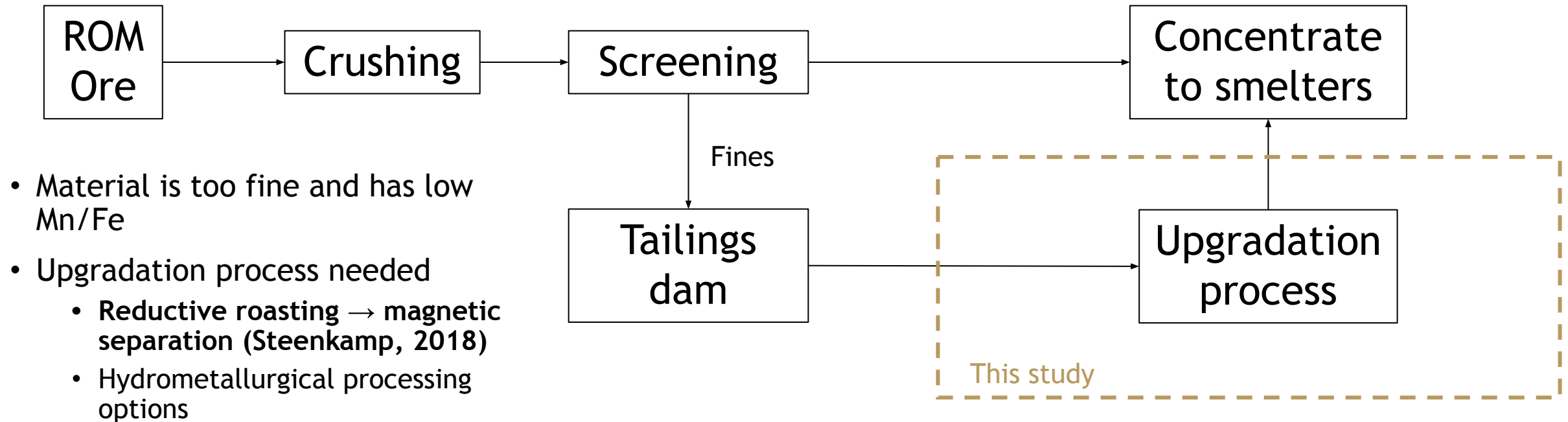
Co-authors: Prof. Margreth Tadie (SU), Prof. Bjorn von der Heyden (SU), and Dr. Robert Cromarty (UP)

Introduction

- Manganese (Mn) has global economic importance
- Used in the ferroalloy industry
 - Smelter feed requires 44% Mn and Mn/Fe >7.5
- Kalahari Manganese Field
 - Largest land-based Mn deposit
 - 70% resources & 38% reserves globally



Simplified Flowsheet



Ties to geometallurgy

- Orebody is highly variable
 - Wide range of Fe content in Mn minerals and Mn content in hematite
 - Geometallurgical models → know what Mn and Fe levels to expect
- Minerals can have unique reduction characteristics
- Statistical modelling useful in predicting behaviour
- Flowsheet design
 - Improve full orebody utilization
 - Reduce carbon emissions

Process selection

- Process can be selectively applied based on geometallurgical domains
 - High Mn/Fe ores → standard beneficiation
 - Low Mn/Fe ores → upgradation required
- Mineralogy can guide operating parameters
- Plan ore blending based on expected output

The problem

- Processing fines from Nchwaning mine
 - Particle size too fine → make briquettes
- Fines contain 44% Mn and Mn/Fe = 2.6
 - Mn grade is acceptable
 - Mn/Fe <<< 7.5
 - Iron needs to be separated from starting material

Iron deportment

 Hematite
 Bixbyite
 Braunite I/II

Manganese deportment

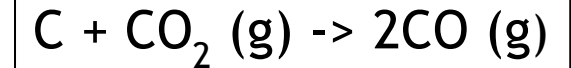
 Braunite I/II
 Bixbyite
 Manganite

XRD - untreated ore

Mineral name	Formula	Mass %
Braunite	$\text{Mn}^{2+}\text{Mn}^{3+}_6(\text{SiO}_4)_8\text{O}_8$	61.0
Hematite	Fe_2O_3	23.2
Manganite	$\text{Mn}^{3+}\text{O}(\text{OH})$	7.9
Calcite	CaCO_3	6.1
Rhodochrosite	MnCO_3	0.7
Birnessite	$(\text{Na}, \text{Ca})_{0.5}(\text{Mn}^{4+}, \text{Mn}^{3+})_2\text{O}_{4.5} \cdot 1.5\text{H}_2\text{O}$	0.7
Magnussonite	$\text{Mn}^{2+}_{10}(\text{As}^{3+}\text{O}_3)_6(\text{OH}, \text{Cl})_2$	0.03

Carbothermic pre-reductive roasting

- The most researched and developed (Larssen et al, 2020)
 - Mn oxides → MnO & Fe oxides → FeO
 - 600 - 800 °C to limit Boudouard reaction
 - CO/CO₂ atmosphere
- Leads to formation of (Mn, Fe)O for ferruginous material (Matabadal, 2022)
 - Difficult to separate
 - Higher temperatures / different reductant required to form metallic Fe
- Large environmental footprint
 - FeMn = 6.1 million tons CO₂ per annum
 - SiMn = 17.5 million tons CO₂ per annum



PARIS2015
UN CLIMATE CHANGE CONFERENCE
COP21·CMP11

Approach

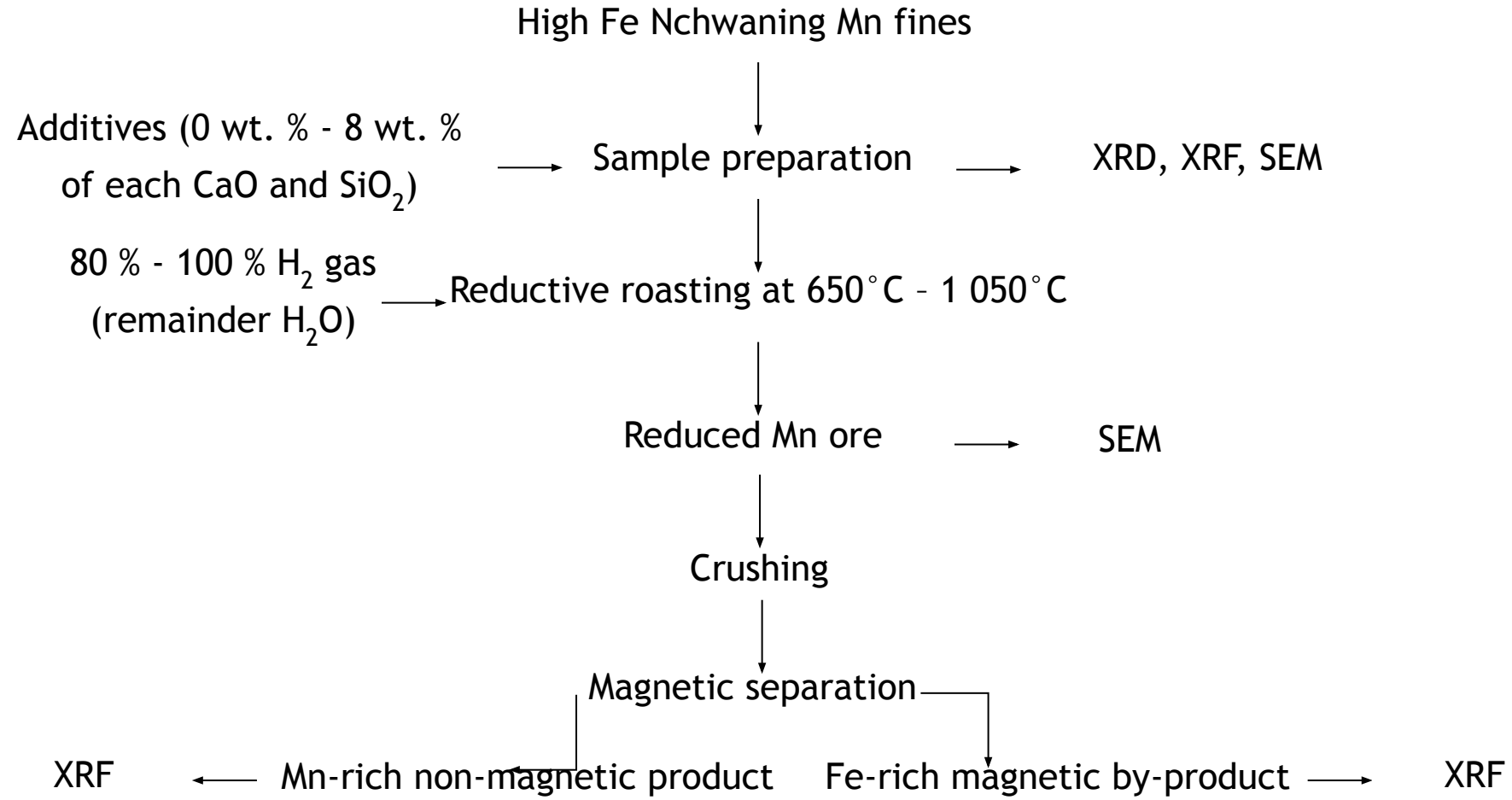
- Different atmosphere (Ernst et al., 2024)
 - H_2/H_2O
 - Pure H_2
- H_2 mixtures = increased extent and rate of reduction
- Pure H_2 more so as well as producing metallic Fe
 - Can be separated magnetically (Kivinen et al., 2010)
- Does not add carbon to the process



Objectives

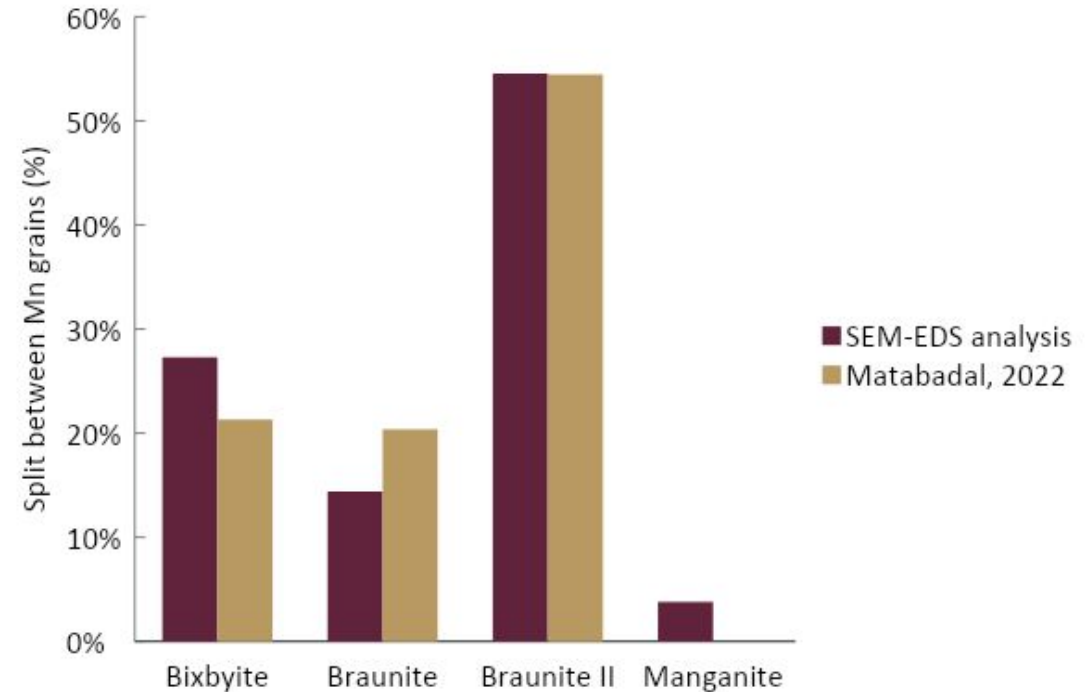
- Develop a beneficiation process for low-grade Mn tailings → hydrogen-rich reductive roasting followed by magnetic separation
 - Produce suitable feed for ferroalloy production
- Investigate optimal working conditions for the chosen process
 - Mn/Fe ratio
 - Mn grade
 - Mn recovery
- Investigate the influence of mineralogical variability on the process

Methodology



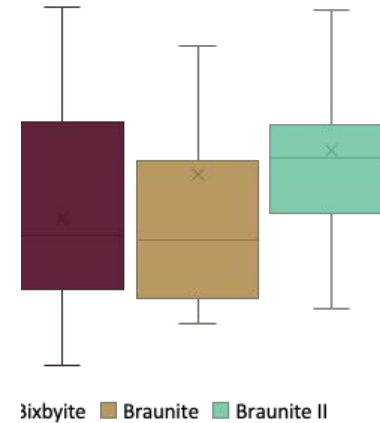
SEM-EDS bulk analysis - Mn minerals

- XRD not able to split between bixbyite, braunite and braunite II
- Applied cation balance and decision tree between major minerals using SEM-EDS data
- Agrees with XRD analysis done on the same fines dump



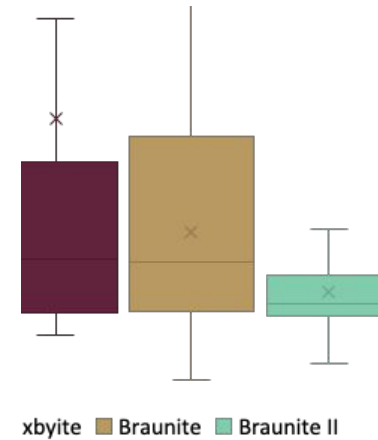
SEM-EDS bulk analysis - Fe content in Mn minerals

- Braunite II is the most abundant and contains the most Fe
- Bixbyite has wide range due to substitution series
- Braunite has the lowest median but a high average due to outliers



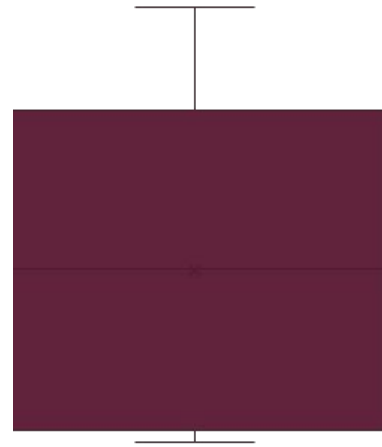
SEM-EDS bulk analysis - Mn/Fe in Mn minerals

- Bixbyite has highest mean Mn/Fe ratio due to a few grains with no Fe
- Braunite II has the lowest as expected
- Braunite with the widest range

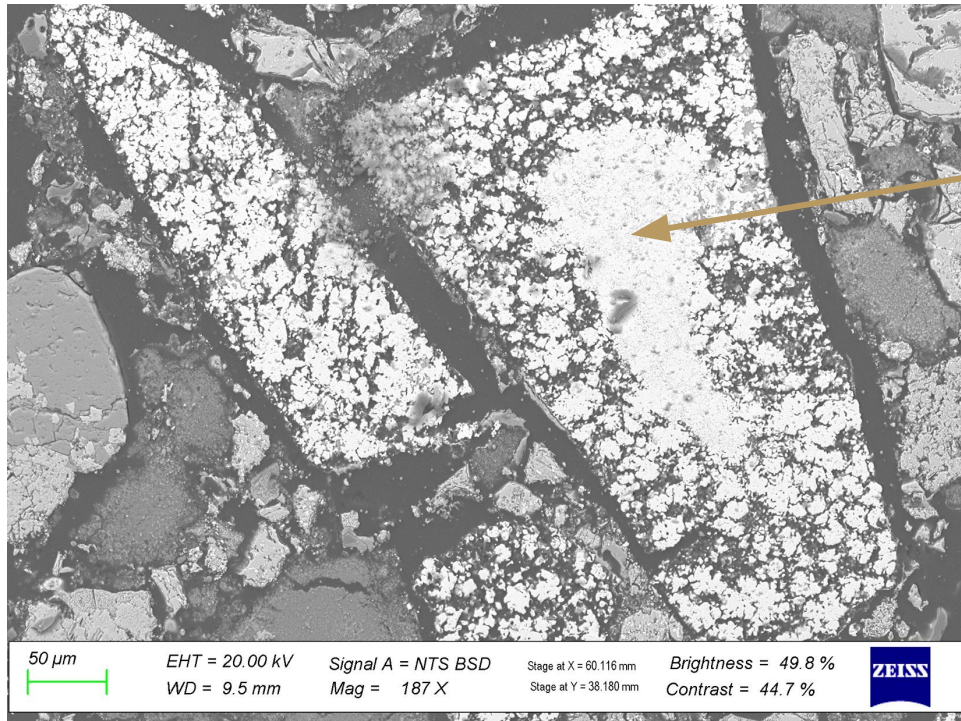


SEM-EDS bulk analysis - Hematite

- 44% of grains analyzed contain < 2 mass % Mn
- Higher levels of Mn will influence activity and reducibility



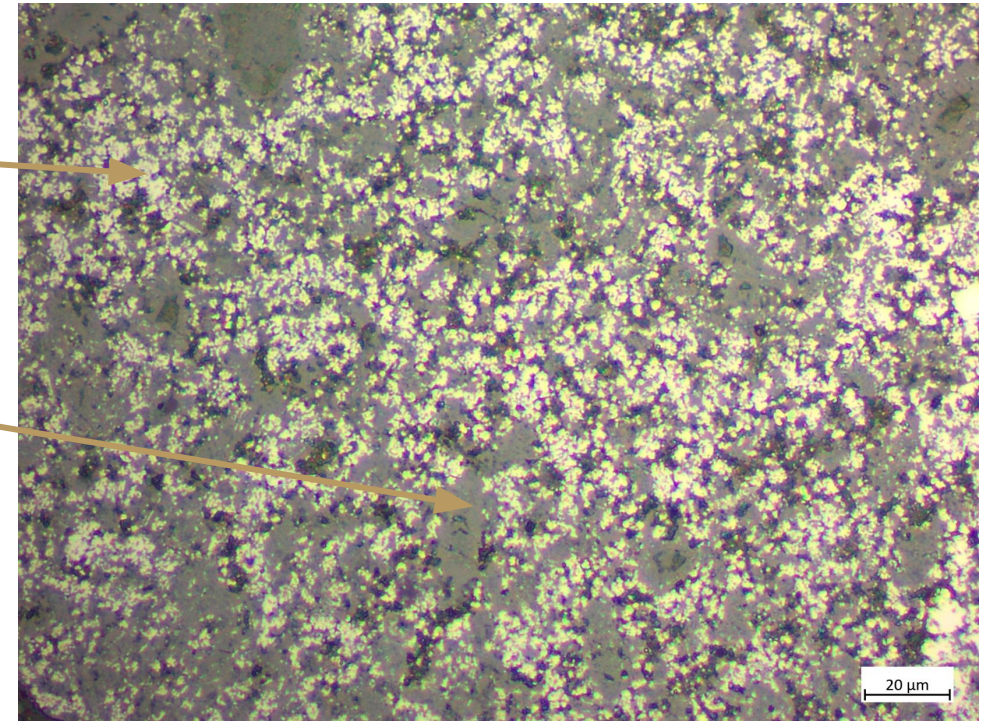
Influence of impurities in hematite reduction



- Fully reduced metallic Fe

Metallic Fe

Mn oxide

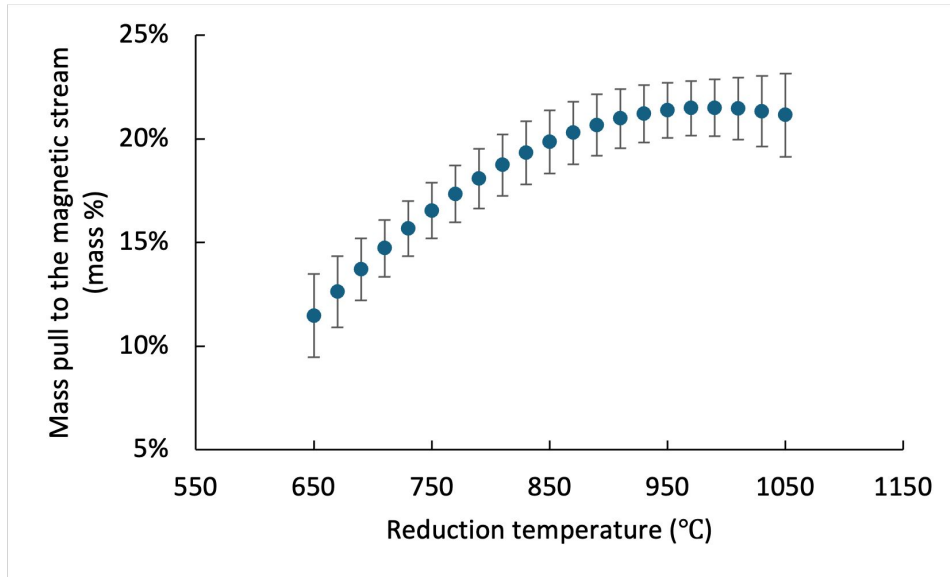


- Partially reduced treated hematite with Mn impurities

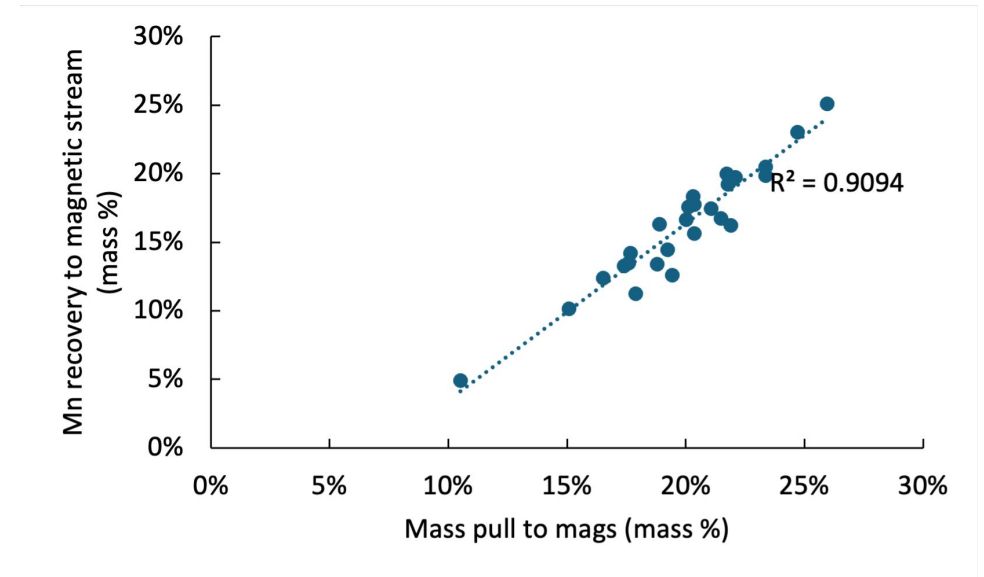
Experimental results

- Mn grade between 50% - 63% ✓
- Mn recovery 73% - 91% ✓
- Mn/Fe ratio 3.43 - 4.52
 - Poor separation between Mn and Fe
 - Why?

Desirability curves- mass pull / Mn recovery

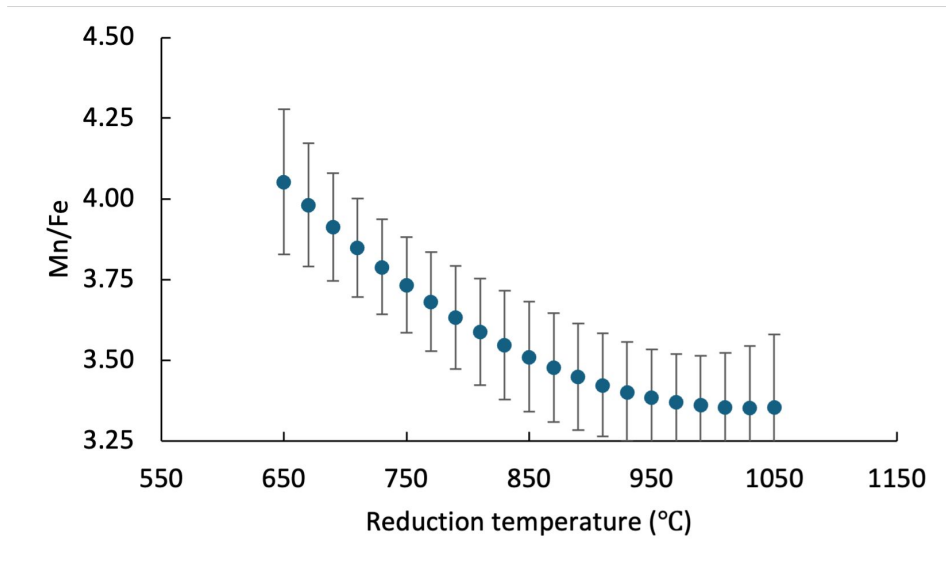


- Levels out due to reduction nearing completion

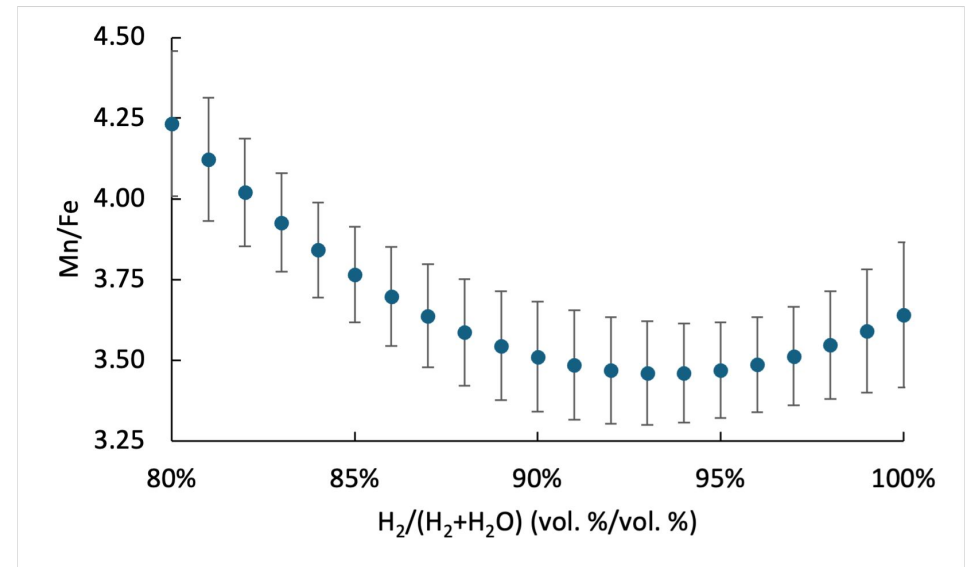


- Mn associated particles reporting to magnetic stream

Desirability curves- Mn/Fe



- Less influence as reduction nears completion



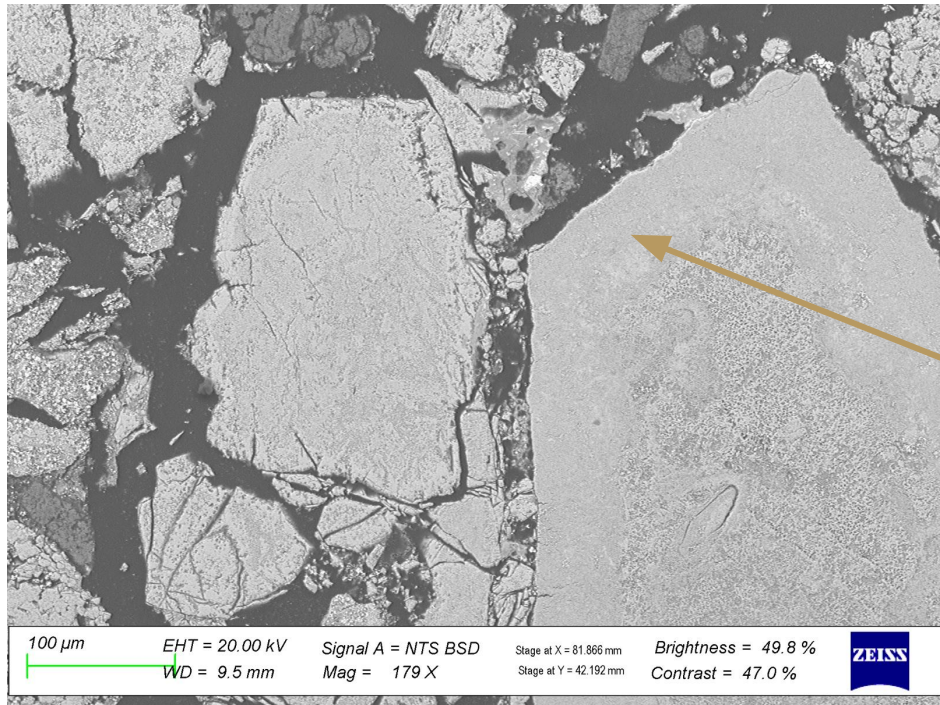
- Uptick at end due to T centre point

Comparison between runs

- Theoretical maximum Mn/Fe achievable = all metallic Fe that forms gets removed perfectly and only oxide is left
- Run 1 had the best overall performance

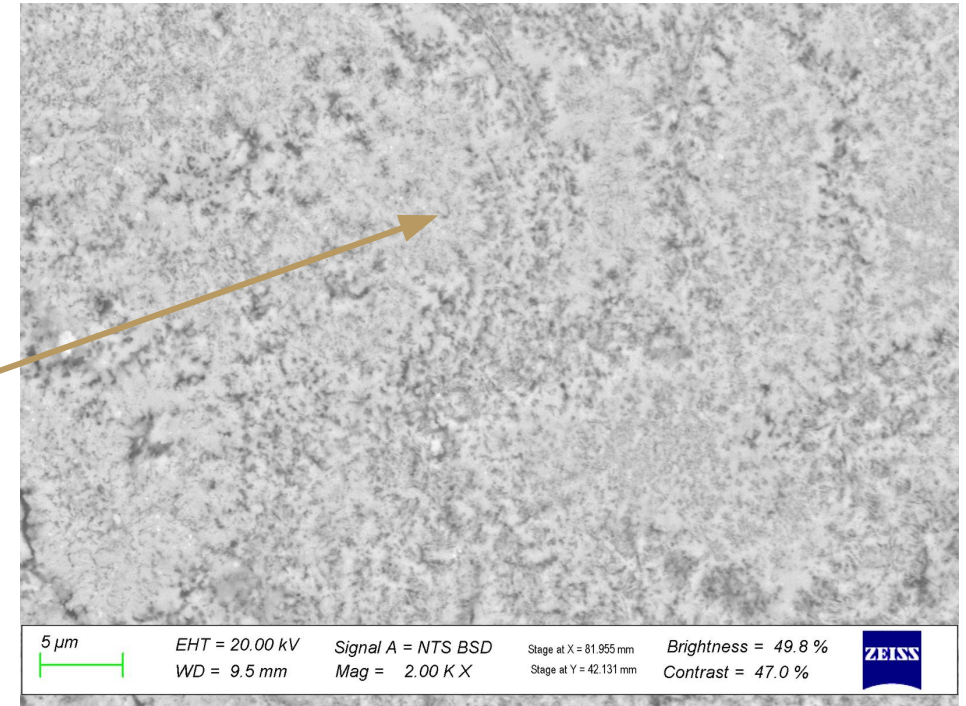
Run	Mn/Fe oxide	Mn/Fe after separation	Percent achieved	
1	5.47	4.52	82.5%	Mildly reducing (750 °C & 85% H ₂)
5	5.11	4.22	82.6%	
16	20.20	3.58	17.7%	New phase forming (950 °C & 95% H ₂)
24	9.42	3.55	37.7%	Full reduction (850 °C & 90% H ₂ / 100% H ₂)
25(C)	10.23	3.53	34.6%	

Highest Fe content with no flecks



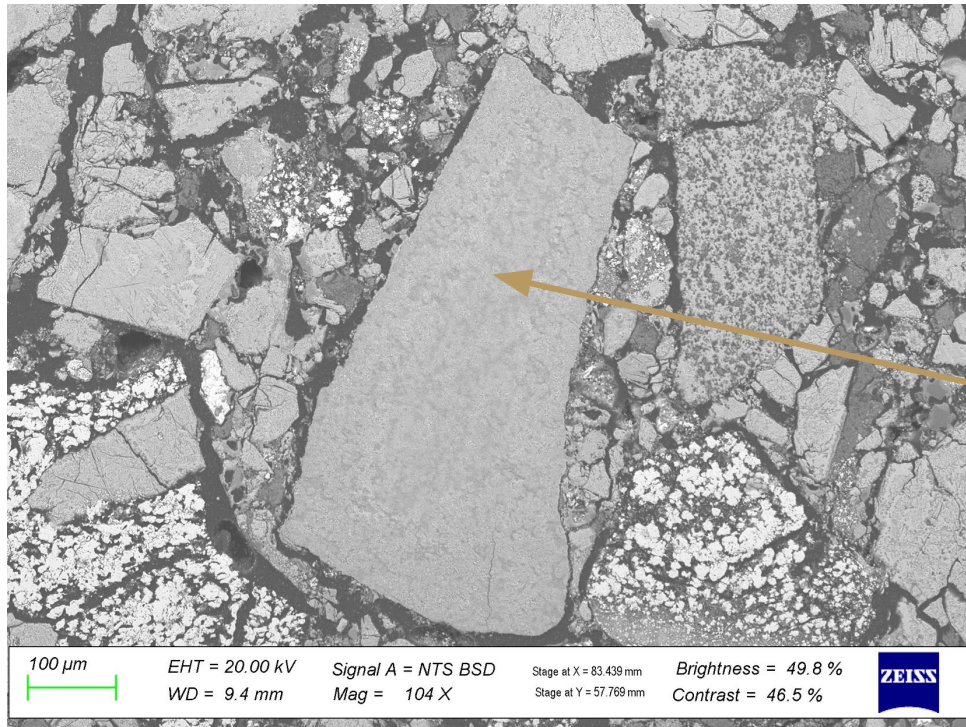
- Mn grain containing 13.1 mass % Fe

Manganosite



- Zoomed in

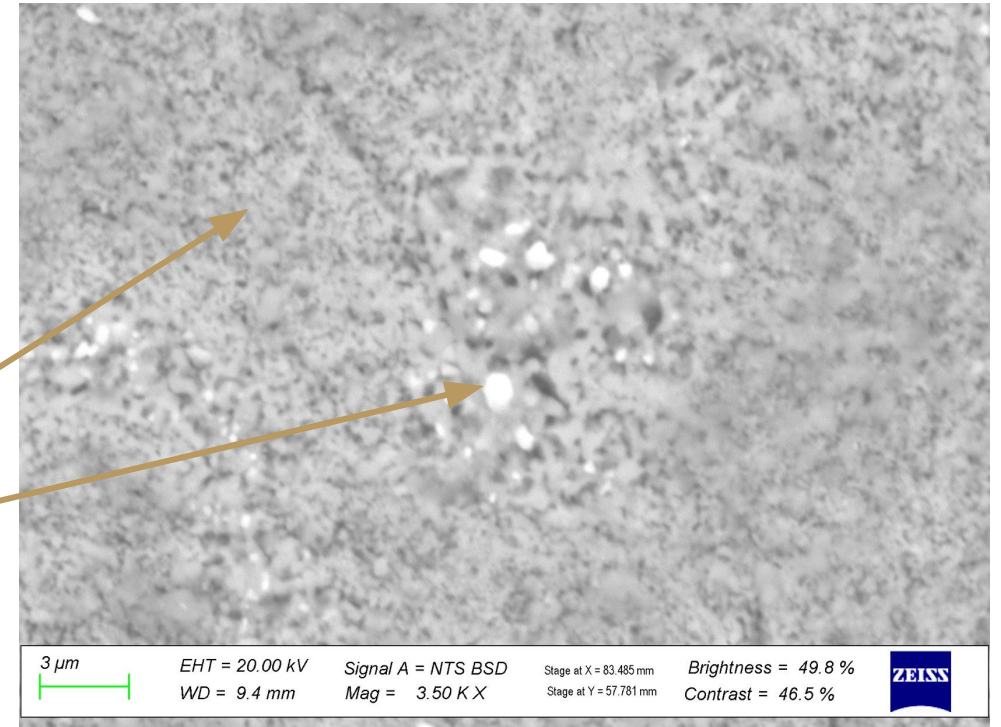
Initial flecks forming



- Mn grain containing 13.6 mass % Fe

Manganosite

Fe alloy



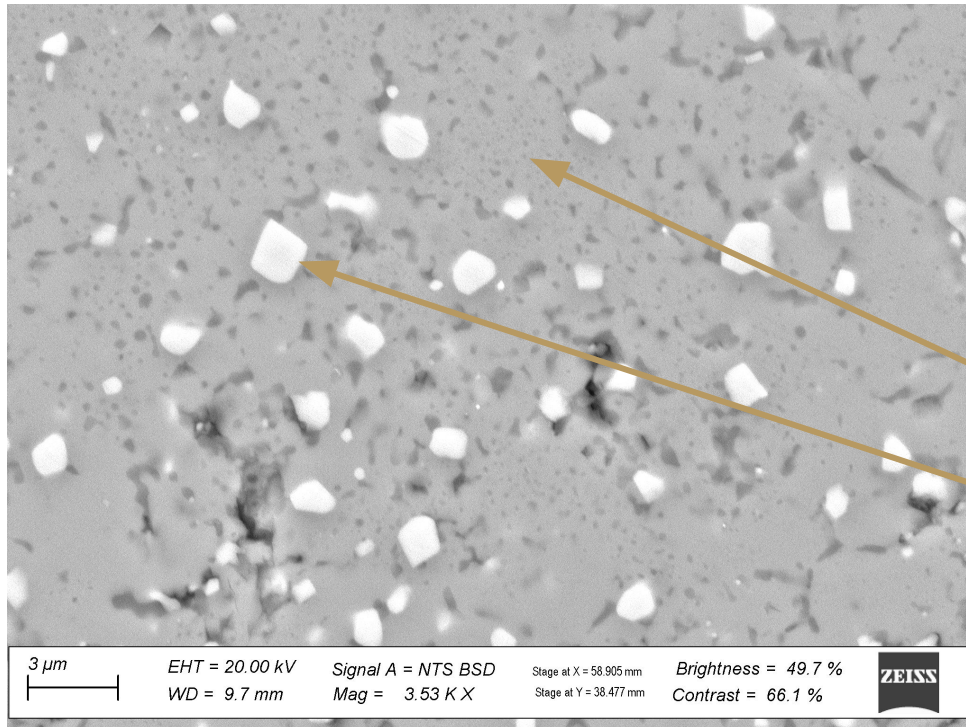
- Zoomed in

How Fe content & reduction conditions influence fleck formation

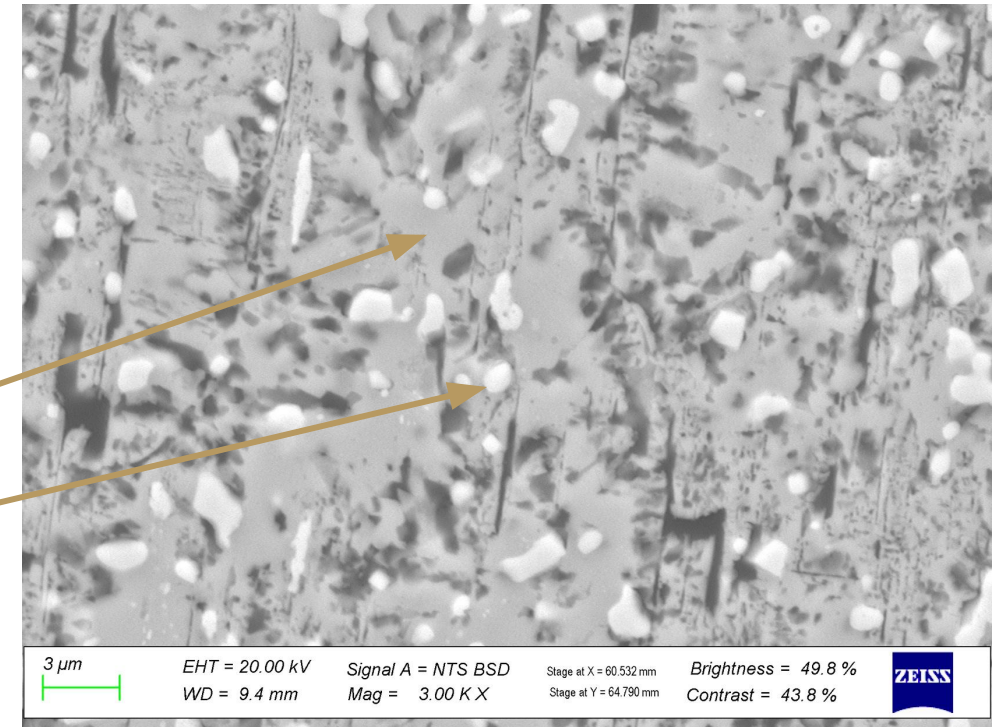
- Requires a higher Fe content to form flecks at milder reducing conditions

Run	Highest Fe bulk without fleck	Lowest Fe bulk with fleck	
1	13.1%	13.6%	} Mildly reducing (750 °C & 85% H ₂)
5	8.6%	16.8%	
17	21.0%	62.2%	} Weakly reducing (650 °C & 90% H ₂)
24	4.0%	7.4%	} Full reduction (850 °C & 90% H ₂ / 100% H ₂)
25(C)	5.4%	7.7%	

Fe alloy flecks in treated bixbyite

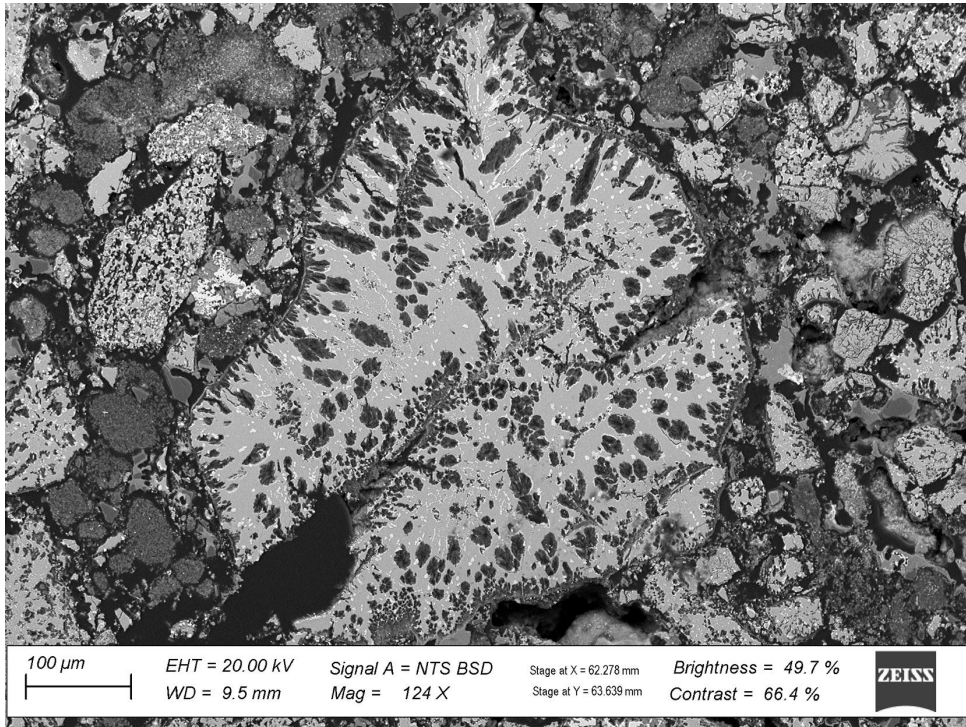


- Treated bixbyite reduced at 950 °C



- Treated bixbyite reduced at 850 °C

Braunite II new texture

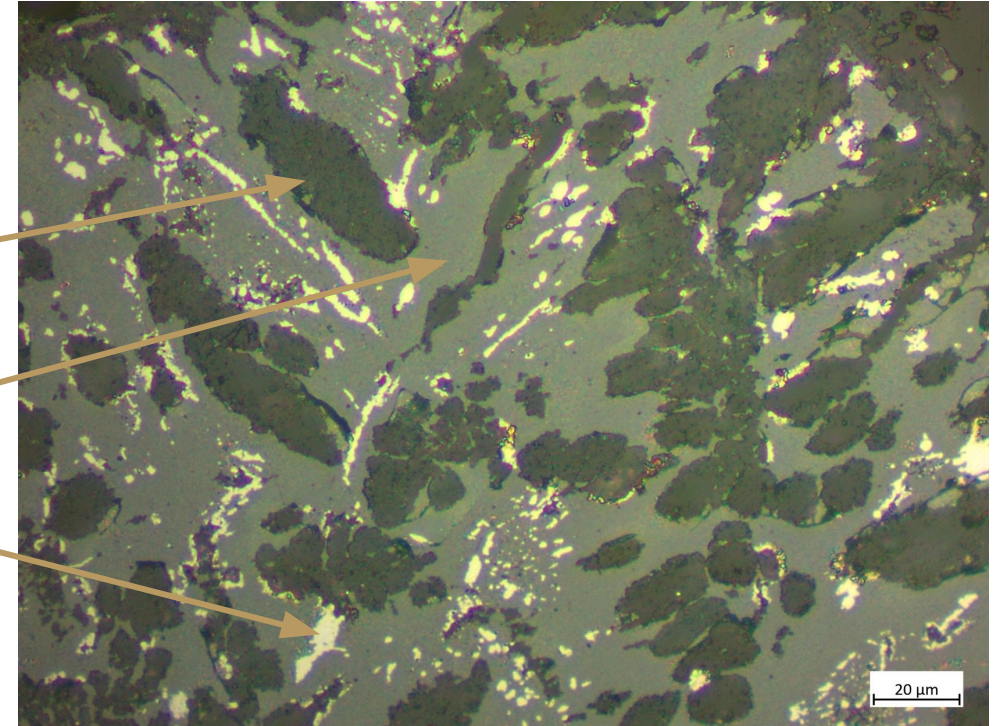


- Reduced braunite II at 950 °C

Mn-Ca silicate

Manganosite

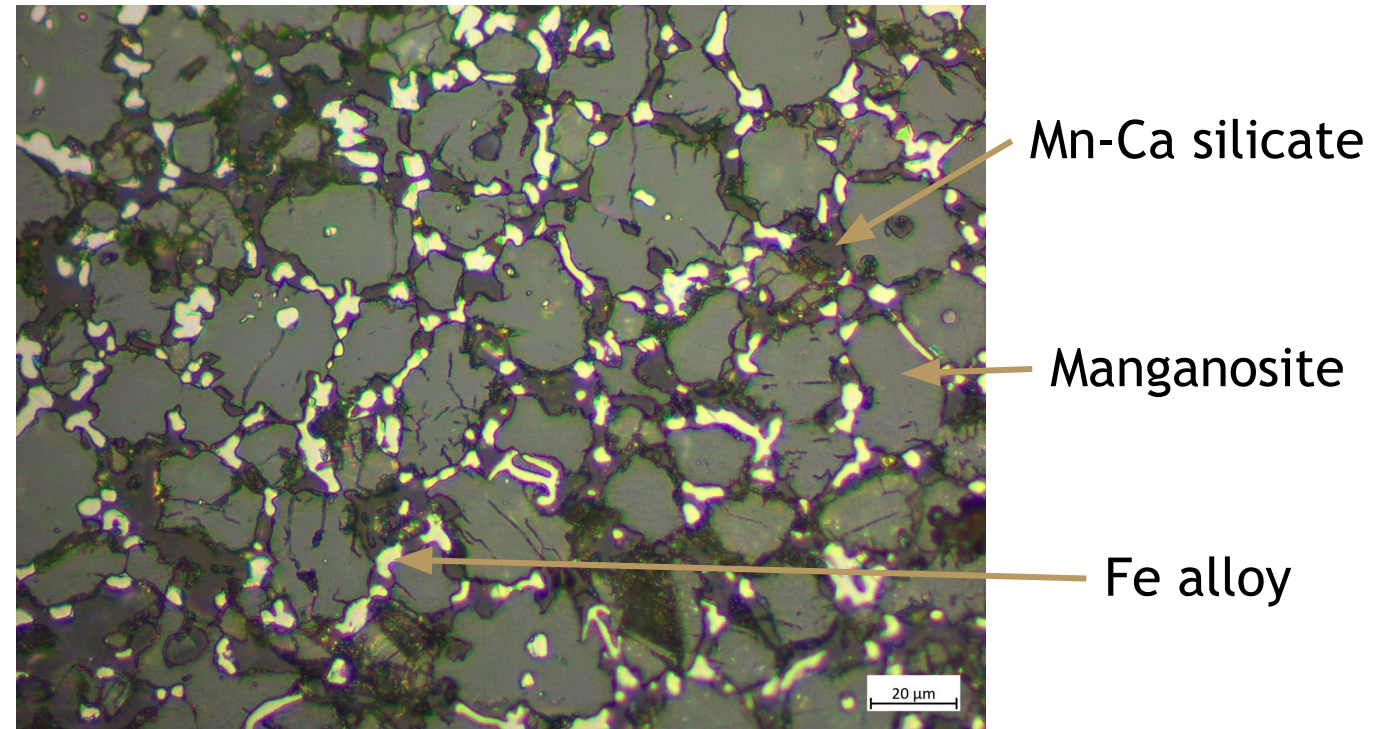
Fe alloy



- Zoomed in using optical microscope

Same grain, increased reduction temperature

- Different texture
- Fe alloys well liberated from manganosite
- Possible to liberate Fe alloys through optimising crushing



Conclusions

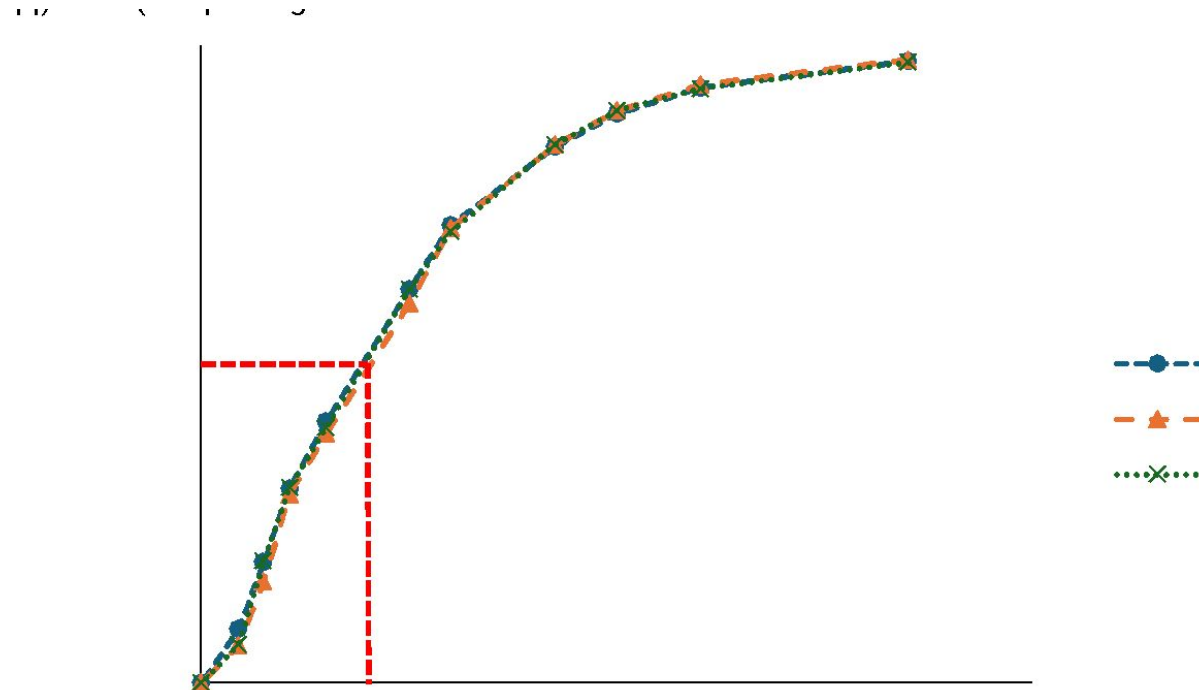
- Hydrogen-rich reductive roasting → magnetic separation upgrades ferruginous Mn fines
 - Mn/Fe too low but can work with blending
 - Liberation and magnetic separation can be improved
- Milder reducing conditions resulted in better separability
- Minerals have unique reduction characteristics
 - Not able to take full advantage in current study

Thank you!

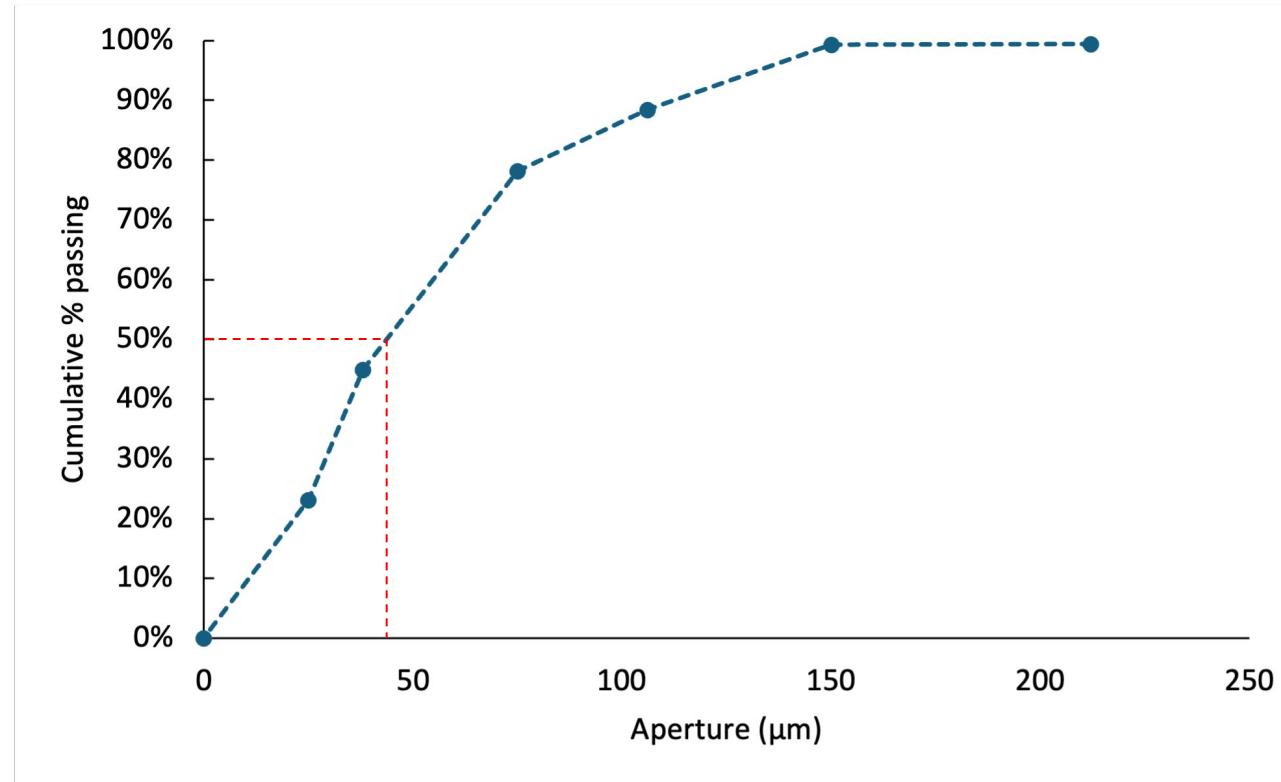
Questions?



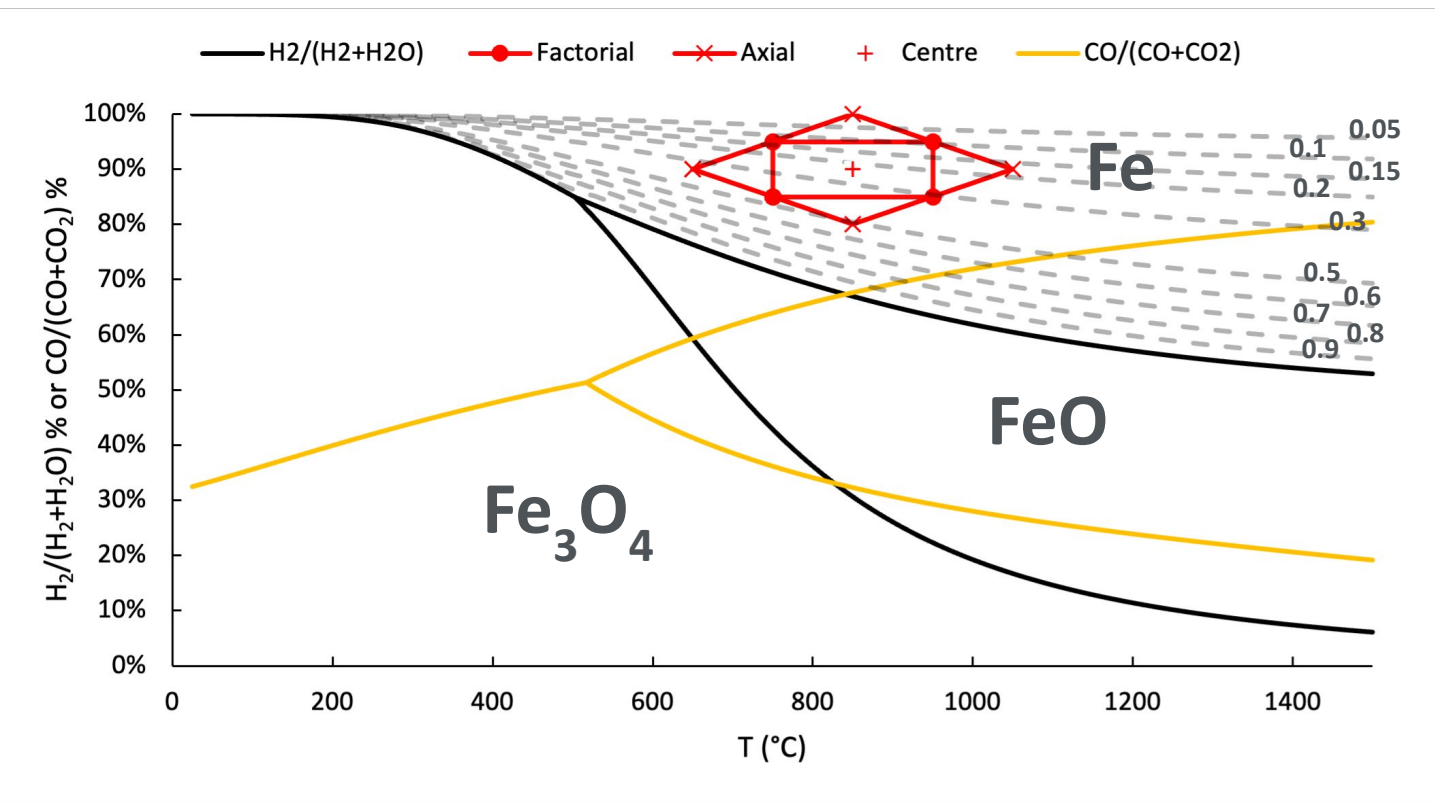
Particle size distribution - untreated



Particle size distribution - reduced and crushed



Iron oxides stability diagram



Back to mineralogy

- Significant differences in Mn/Fe possible for different minerals
 - Higher Mn/Fe for Braunite II at higher temps once new structure forms
- Not achieved in current study due to limits of liberation and magnetic separation
 - Improvement is possible

Mineral	Tailings Mn/Fe	Mn/Fe oxide
Bixbyite	7.88	9.02
Braunite	5.47	7.84
Braunite II	4.85	11.45